

CFD modelling of liquid pressurized water and phase change through leaks in micro-cracks

Quantitative estimates - comparison with analytical solutions

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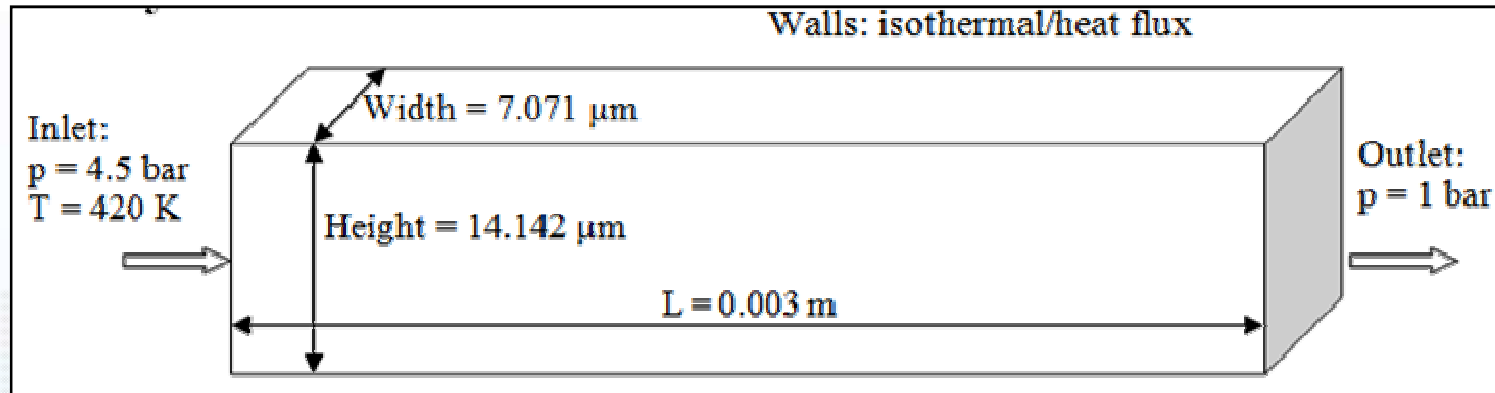
Introduction (1)

- Vapour leak in the vacuum vessel of ITER
- Detection of leaks and determination of the fastest method to pinpoint the leak location
- FLUIDYN mandated for 2 tasks :
 - Model the spatial distribution of water vapour from a leak in the BSM according to the leak type, operational state and location
 - **Model the liquid water behaviour flowing through a crevice into the vacuum according to the type of crevice**

Introduction (2)

- Preliminary studies :
 - Analytical tool based on Sharipov (99) and Sharipov et al (2010)
 - CFD modeling of He flowing into crevice (pure gas+ heat exchange)
- CFD modeling for water leaks (with phase change)
 - Use of Homogeneous Equation Model (HEM)
 - 4 cases :
 1. Isothermal fluid : all heat needed is available
 2. Isothermal wall boundary : maximum heat from the wall
 3. Adiabatic wall boundary : no heat from the wall
 4. Conjugated Heat Transfer (1D) in the wall : more realistic

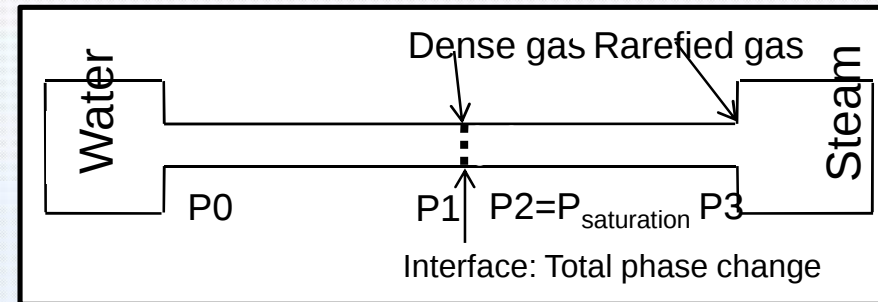
Geometry and case definition



- Length of 3 mm or 1cm depending on case
- $H/w = 2$
- Inlet pressure of $4.5\text{E}+05 \text{ Pa}$
- Outlet pressure of $1.0\text{E}+05 \text{ Pa}$
- Rarefaction parameter at outlet $\delta \sim 80$
- Temperature of fluid (or wall) = 420 K
- Computational domain : $\frac{1}{4}$ of the cross-section
- 16000 hexahedral elements.

Brief description of the analytical tool

- Sharipov model :
 - Isothermal flow
 - Total evaporation
 - Laminar liquid flow
 - Sharp interface between liquid and steam
 - Whole range of rarefied gas (slip to free molecular regime)



- Methodology :
 - Initialization : First guess of the mass flow rate
 - Based on rarefied gas solution, pressure profile upstream reconstructed up to the saturated pressure. Gaseous and liquid lengths estimated.
 - Liquid mass flow rate from Poiseuille solution estimated with liquid length.
 - Convergence criteria: balance between liquid and gas flow rate.

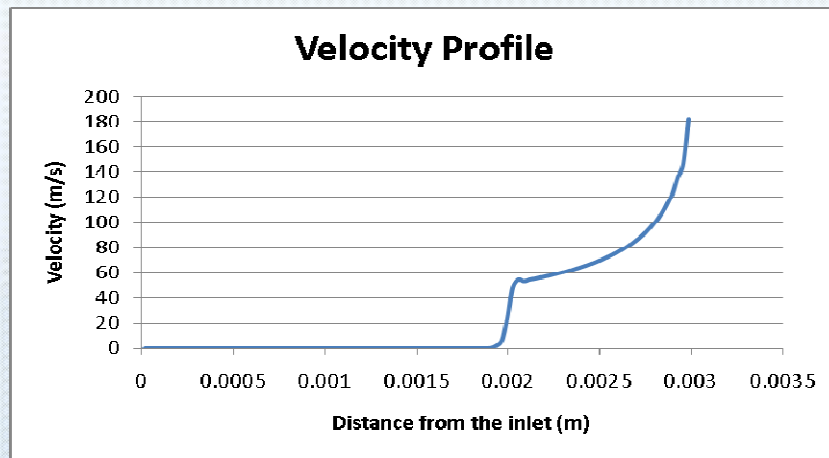
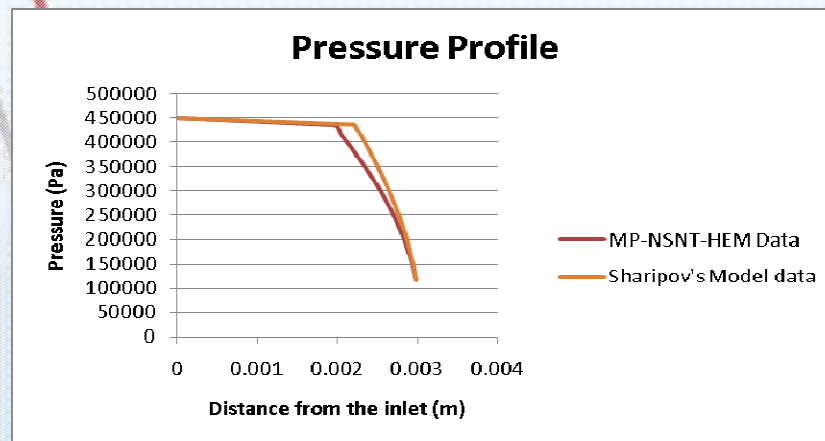
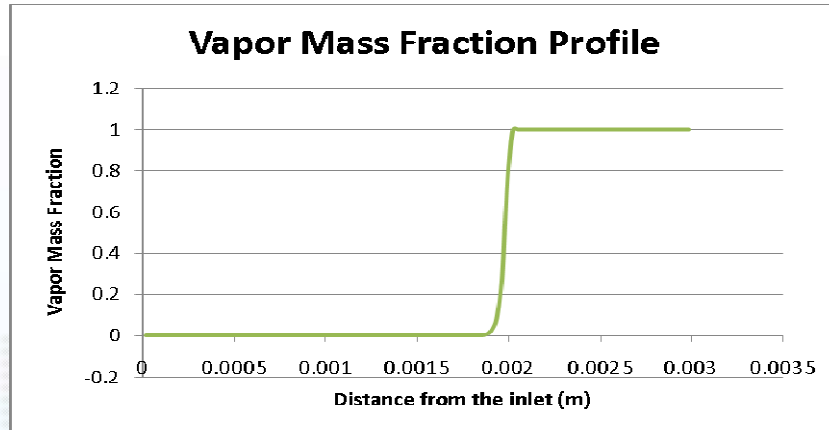
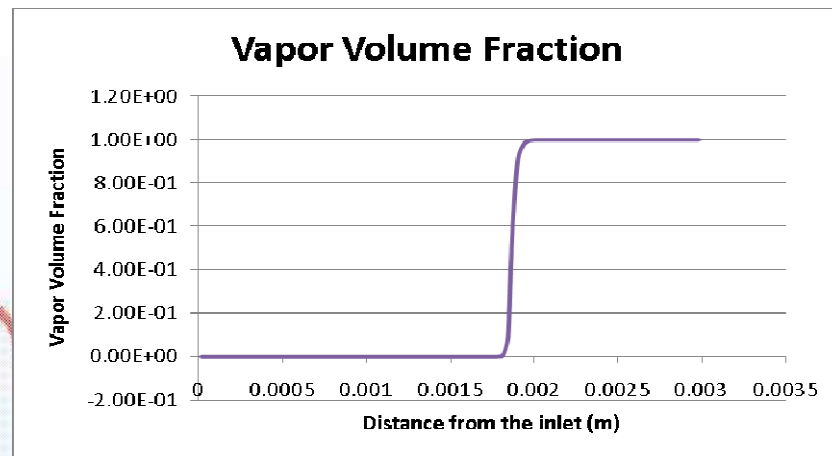
Fluidyn-MP-NSNT

Equation for mixture	EOS
$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{U}) = 0$ $\frac{\partial (\rho \mathbf{U})}{\partial t} + \nabla \cdot (\rho \mathbf{U} \mathbf{U}) = \nabla \cdot \boldsymbol{\tau} - \nabla p + S_{\mathbf{U}}$ $C_p \left[\frac{\partial (\rho T)}{\partial t} + \nabla \cdot (\rho \mathbf{U} T) \right] = \nabla \cdot \mathbf{q} - \left[\frac{\partial (\ln \rho)}{\partial (\ln T)} \right]_p \left[\frac{\partial p}{\partial t} + \mathbf{U} \cdot \nabla p \right] + S_T$ Transport equation for the gas phase $\frac{\partial (\rho \phi)}{\partial t} + \nabla \cdot (\rho \mathbf{U} \phi) = \nabla \cdot \mathbf{J} + S_{\phi}$	$p = \frac{T \sum_i^{i \neq h2ol} R_i \rho_i}{\theta} = \frac{\rho T \sum_i^{i \neq h2ol} R_i X_i}{\theta}$ Source term for evaporation $S_{h2og} = \frac{(\rho_{sat} - \rho_{h2og, gas})}{t_{pc}}$

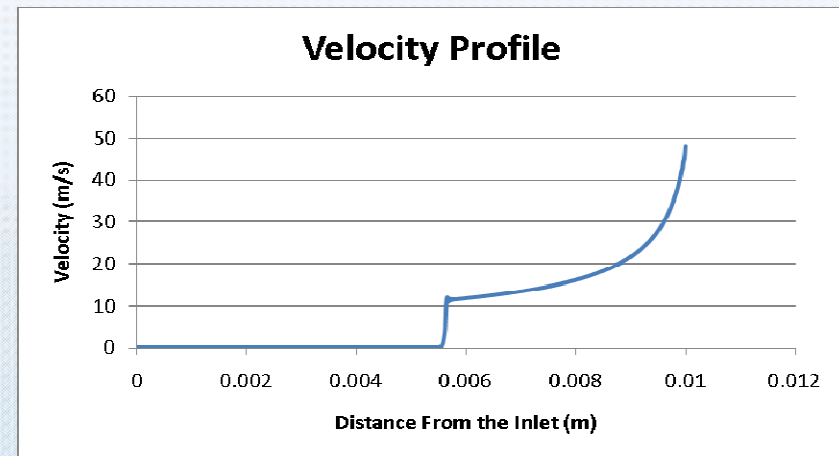
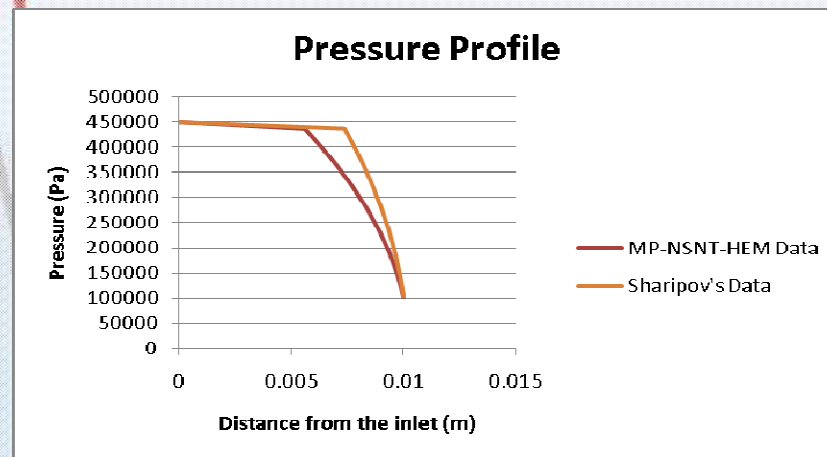
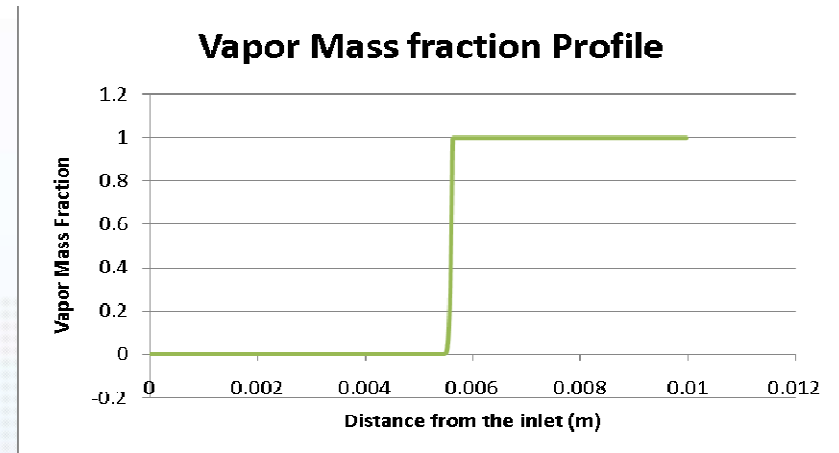
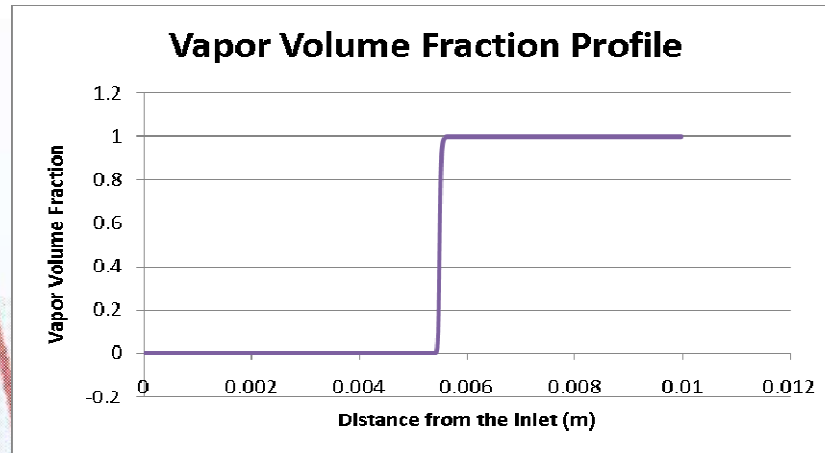
Boundary Conditions:

- Inlet: Liquid+ 10-8 mass fraction of gas
- Outlet: Open at pressure 1bar
- Structure: Adiabatic or isothermal or solution 1D conduction heat transfer in steel

Results for isothermal fluid for 3mm tube *fluidyn* FRANCE



Results for isothermal fluid for 1cm tube



Isothermal fluid case

	Mass flow rate (kg/s)		Distance to Psat (m)	
	Sharipov	HEM	Sharipov	HEM
3mm	1.2E-08	1.13E-08	2.21E-03	1.97E-03
1cm	3.7E-09	2.55E-09	7.37E-03	5.51E-03

- CFD-HEM and analytical solution are matching.
- Differences may be due to:
 - non-slip conditions for this case (rarefaction order of 100).
 - different EOS laws for both $P_{\text{sat}}(T)$ and viscosities(T) liq and gas.

Thermal budget

A Posteriori analysis of energy requirement:

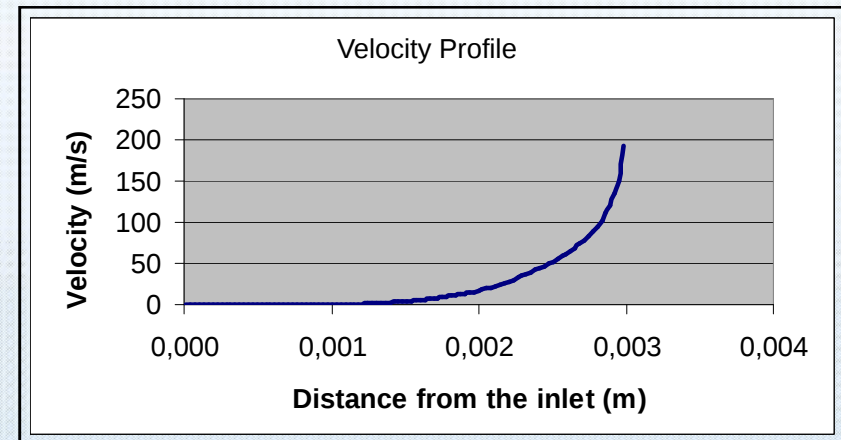
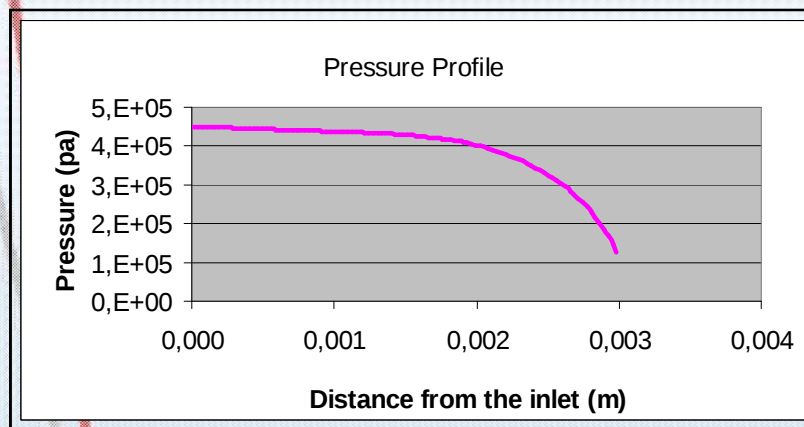
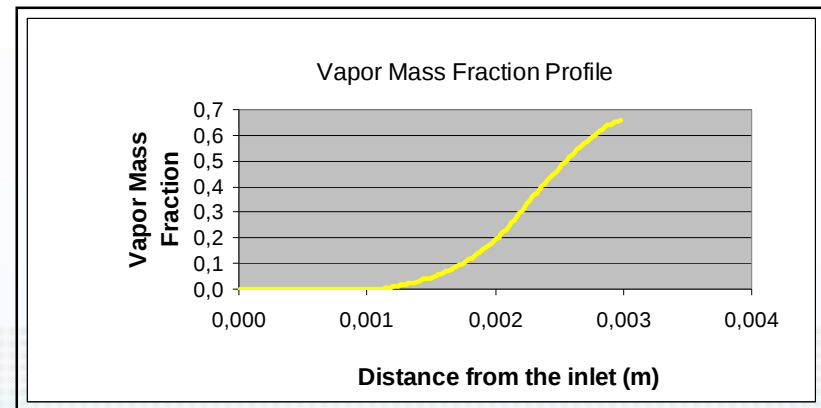
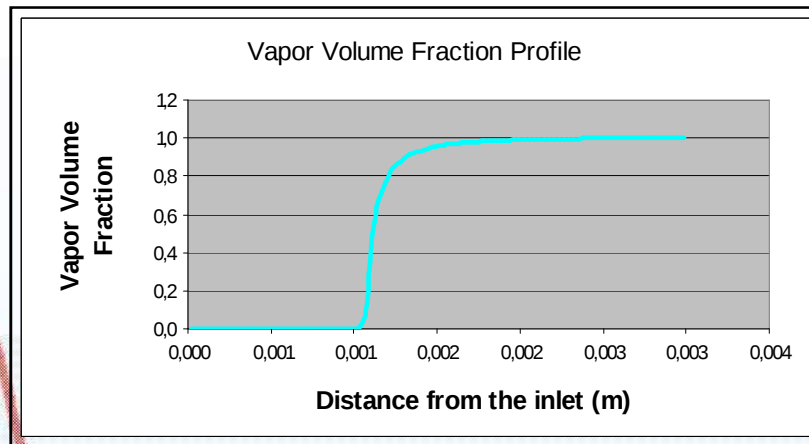
- Mass flow rate $Q_m = 1.2 \cdot 10^{-8} \text{ kg/s}$
- Heat for evaporation $L_v = 2.1 \cdot 10^6 \text{ J/kg}$
- $Q_w = 0.0256 \text{ W}$ to be distributed on a equivalent surface (of wall)
- $S = 42 \times 10^{-6} \text{ m} \times 0.003 \text{ m} = 0.126 \cdot 10^{-6} \text{ m}^2$
- Average surface heat flux to be injected = **203 kW/m^2**

Can the Wall provide such heat flux (even worse on a sharp interface) ????

➤ ***Analysis with 3D CFD HEM and heat transfer in fluid and structure***

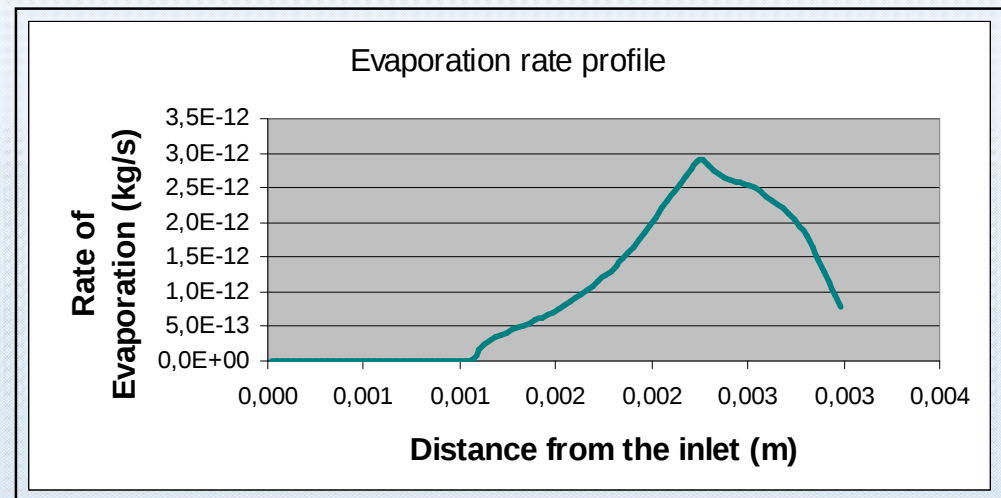
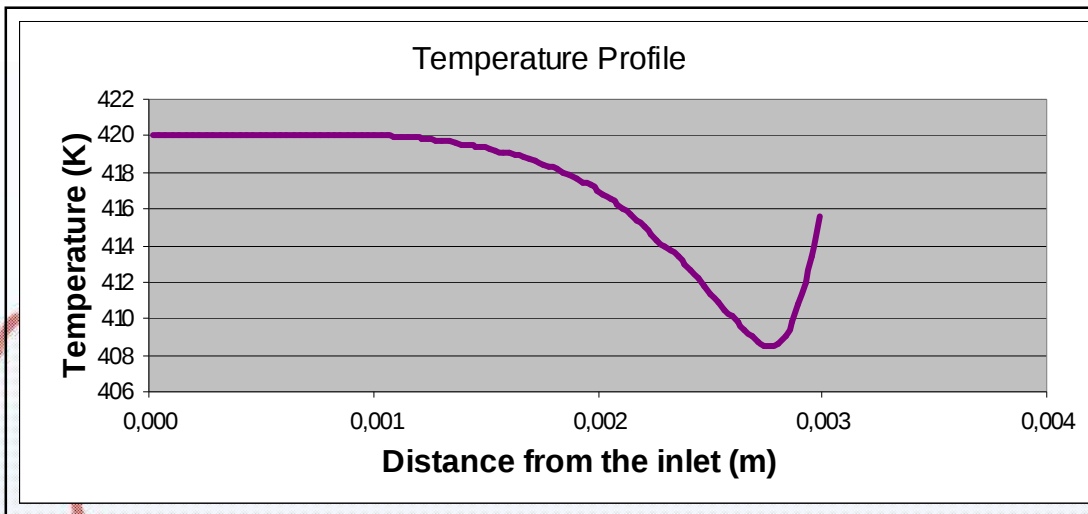
- Isothermal wall boundary (maximum heat flux from wall)
- Adiabatic wall boundary (no heat flux from wall)
- Conjugated Heat Transfer (1D-CHT) in the wall (conduction limited heat flux from wall = most realistic)

Results for isothermal wall (1/2)

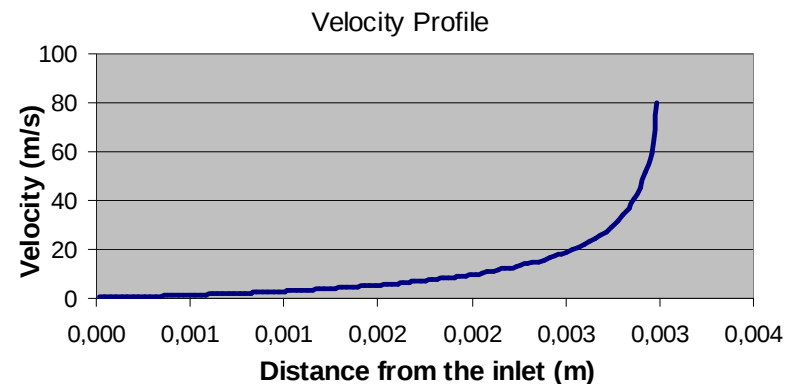
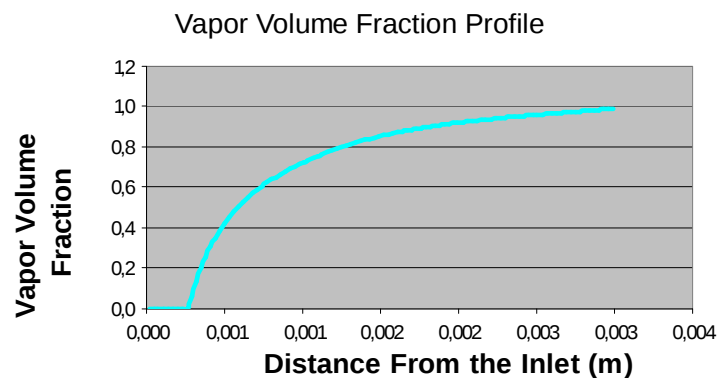
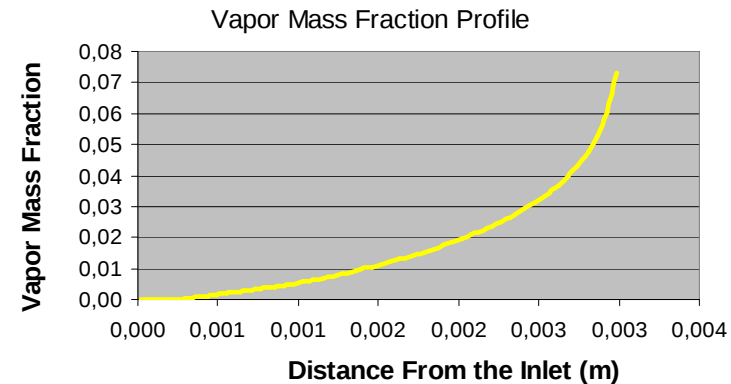
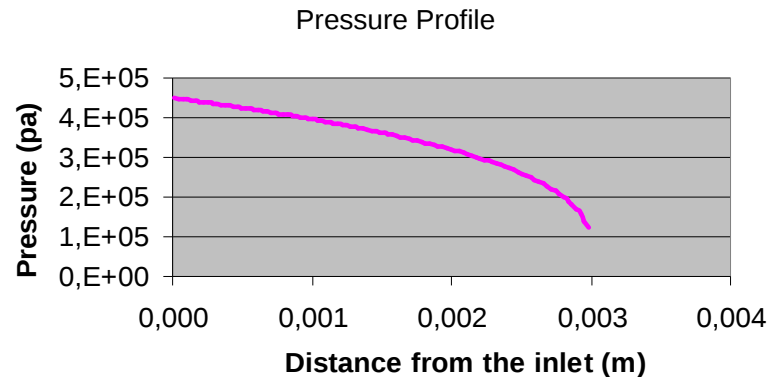


- Sharp Interface lost, pressure drop smoother, 30% mass fraction of liquid at outlet
- In relation with temperature drop (not maintained by heat flux from wall)

Results for isothermal wall (2/2)

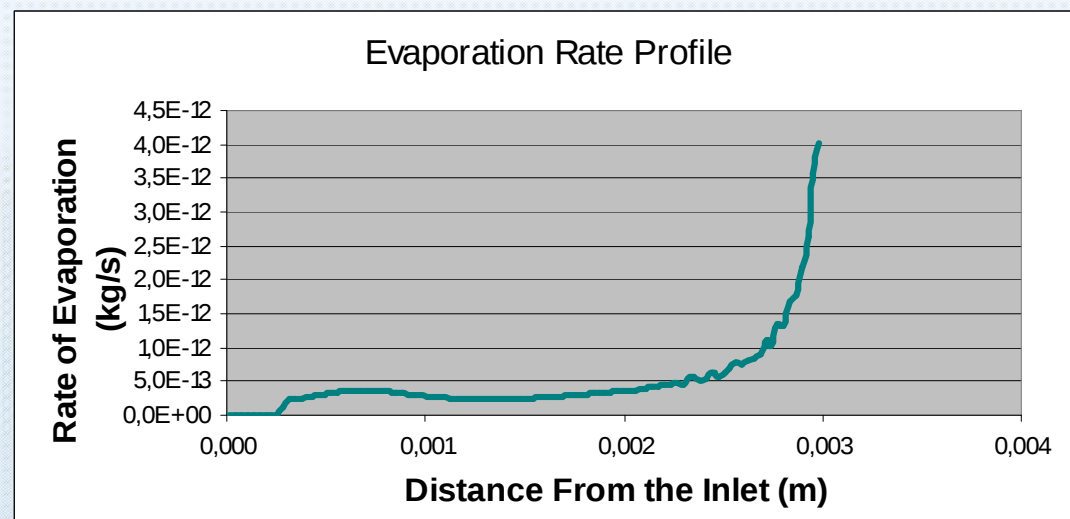
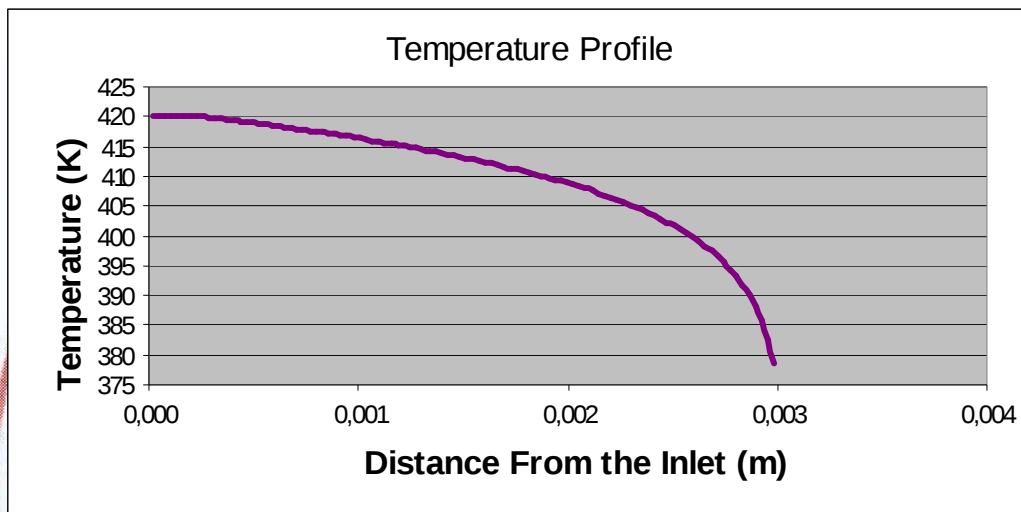


Results for adiabatic wall (1/2)

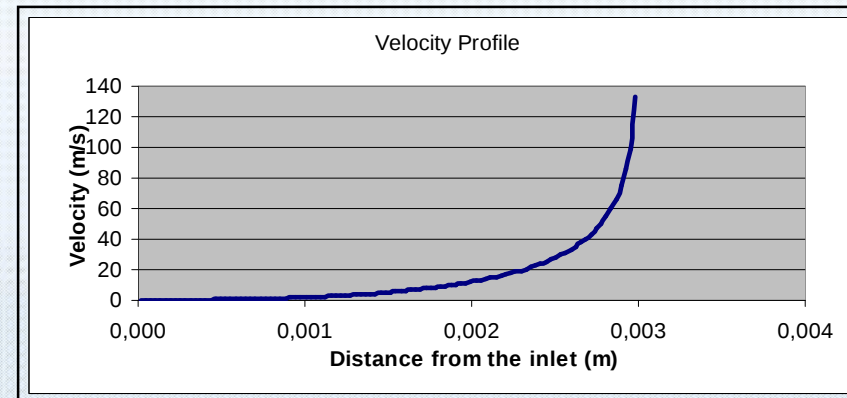
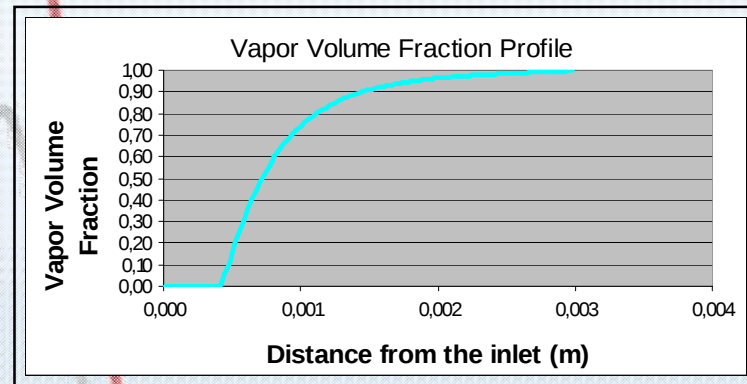
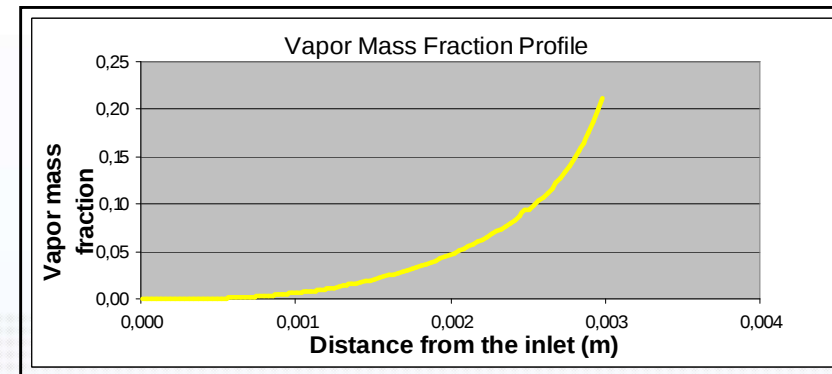
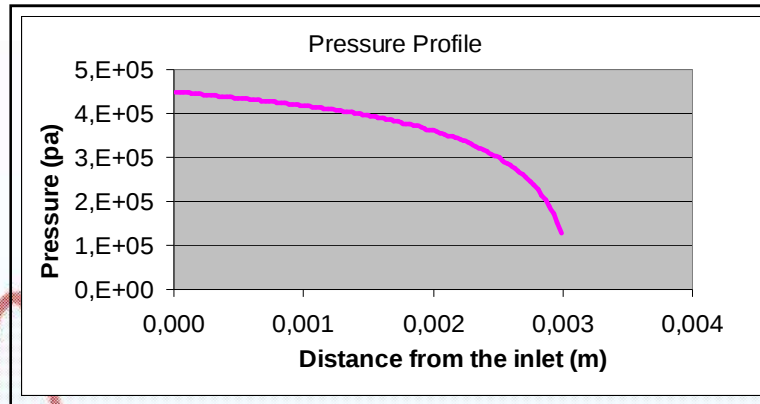


- Sharp Interface lost, pressure drop smoother, 93% mass fraction of liquid at outlet
- In relation with strong temperature drop (latent heat pumping and no heat at all from the wall)

Results for adiabatic wall (2/2)



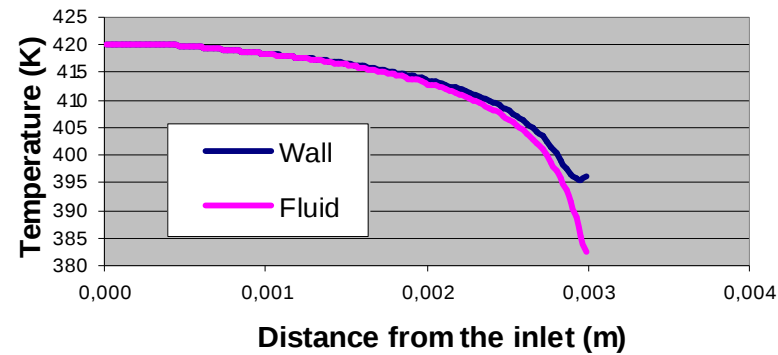
Results for conducting wall (1/2)



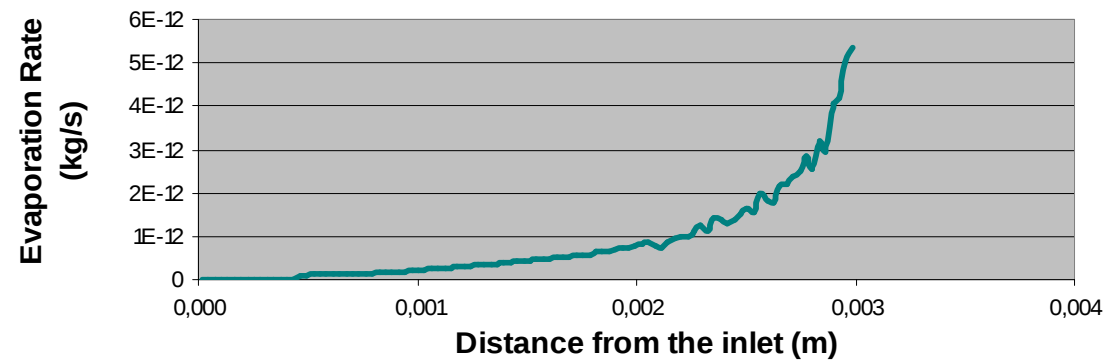
- Sharp Interface lost, pressure drop smoother, 80% mass fraction of liquid at outlet
- In relation with strong temperature drop (limited heat from wall conduction)
- Results at 70ms transient: wall keeps on cooling

Results for conducting wall (2/2)

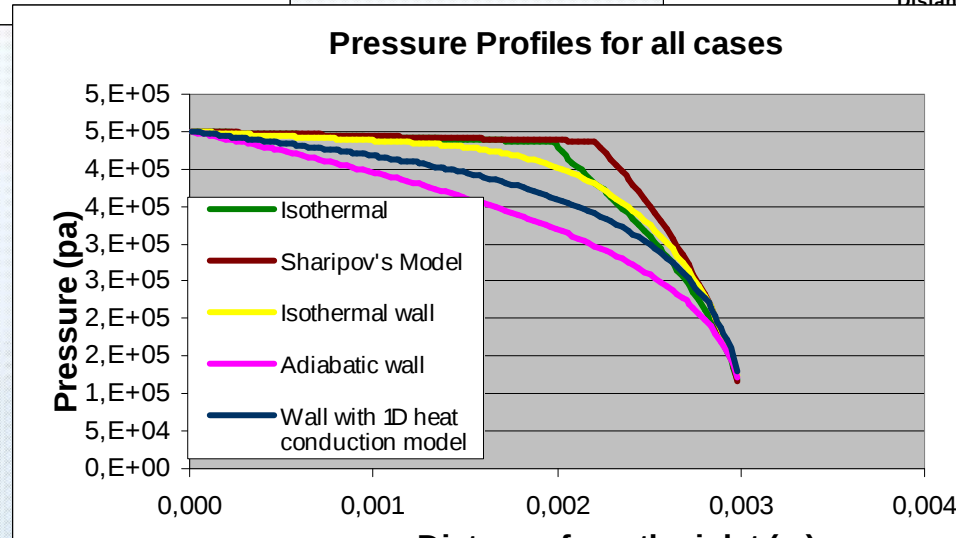
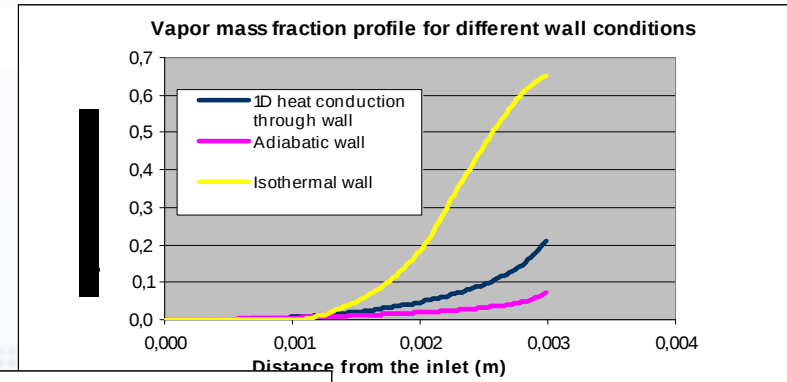
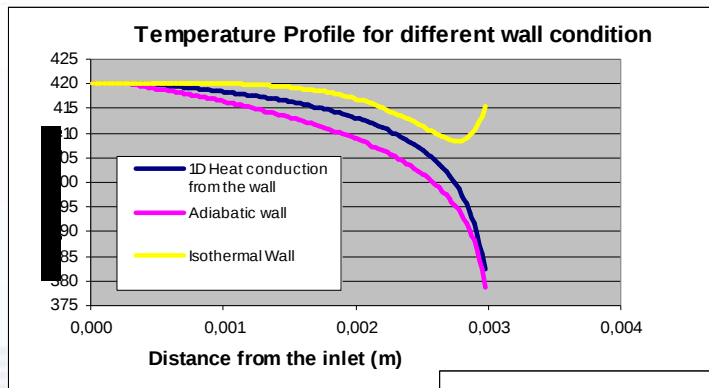
Temperature Profile



Evaporation Rate Profile



Comparison of all non-isothermal cases



CFD-HEM adiabatic (kg/s)	CFD-HEM 1D heat conduction (kg/s)	CFD-HEM isothermal wall (kg/s)	CFD-HEM isothermal flow (kg/s)	Sharipov's model (kg/s)
8.0E-08	4.96E-08	1.98E-08	1.13E-08	1.2E-08

- In similar conditions, fair agreement of CFD-HEM with Sharipov's model.
- For non-isothermal flows :
 - mass flow rate higher than isothermal flow.
 - only partial evaporation
- 1D heat conduction between that of the isothermal wall and adiabatic case.
- Area of phase change ?
- ITER cases